Town of Kent

Town Board Meeting

September 19, 2023

Workshop/Meeting

1. Pledge of Allegiance
2. Roll Call
3. Discussion and/or Vote on the following:
    a. Assessor- discussion of Public Reappraisal
    b. NY Forward- listening session
    c. South Lake- dam project
    d. Code Enforcement- violation
    e. Highway-advertise for laborer
    f. Police Department- repeater, fence
    g. Lake Carmel FD- retirement program
4. Vouchers
5. Announcement
6. Public Comment

Basis of Design Report

Upper and Middle South Lake Dams

Prepared for

Putnam County

1 Geneva Road

Carmel, New York

Revision 0

July 2023

Barton&Loguidice

Upper and Middle South Lake Dams
Putnam County

Basis of Design Report

July 2023

Prepared for

Putnam County

1 Geneva Road

Carmel, New York 10512

Prepared by

Barton & Loguidice, D.P.C.
443 Electronics Parkway
Liverpool, New York 13088

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Appendices

ABBREVIATIONS

cfs	Cubic feet per second
DEC	New York State Department of Environmental Conservation
LiDAR	Light detection and ranging
NOAA	National Oceanic and Atmospheric Administration
SDF	Spillway design flood
USACE	United States Army Corps of Engineers

1.0 BACKGROUND

Putnam County Soil & Water Conservation District (County) has tasked Barton & Loguidice (B&L) to evaluate a potential permanent breach of the Upper and Middle South Lake Dams. The goal of the project is to reclassify one or both dams to Class 'D' (breached) or Class 'A' (low hazard) to reduce inspection and maintenance requirements for the structures. This assessment includes the development of detailed hydrologic studies and concept design plans showing the scope of the recommended breach alternative.

This detailed assessment includes analysis applicable to the following three dams:

- Upper South Lake (DEC Dam ID 230-5708)
- Middle South Lake (DEC Dam ID 230-0571)
- Lower South Lake (DEC Dam ID 230-5707)

2.0 HYDROLOGIC MODELING

B&L prepared detailed hydrologic models for the Upper, Middle and Lower South Lakes using the U.S. Army Corps of Engineers' Hydrologic Modeling System version 4.1.0 (HEC-HMS). The basis for the hydrologic models for both the Upper and Middle lakes were obtained from Appendix F of the Draft Engineering Assessment Reports previously prepared by The Chazen Companies in February 2013. B&L reviewed the hydrologic model reports and calculations in the Engineering Assessment Reports and did not find any significant issues with the model approach. Therefore, the same hydrologic methods were followed for the breach assessment.

Minor edits to the original model data included:

- Simplification of the dam crest cross sections obtained from the original Engineering Assessment Reports to meet HEC-HMS formatting requirements; and
- Replacement of rainfall depths with current data obtained from NOAA's Precipitation Data Frequency Server.

The Lower South Lake dam was added to the model using a combination of publically available LiDAR elevation, soil map and land cover data, dam data maintained by the DEC, and new topographic survey data from the Lake Louise Drive culvert replacement project. The results model is the assumed baseline existing condition for all three lakes. A summary of the hydrologic model results and Spillway Design Flood (SDF) criteria is provided in **Table 2-1**. HEC-HMS model reports are provided in **Appendix A**.

Table 2-1: Baseline Hydrologic Model Results

Reservoir/Dam	100-Year Return Peak Inflow (cfs)	100-Year Return Peak Discharge (cfs)	100-Year Return Peak Elevation (ft.)	Spillway Design Flood Discharge (150% of 100-Year) (cfs)
Upper South Lake	721	533	791.7	800
Middle South Lake	631	520	788.8	780
Lower South Lake	622	413	784.4	620

Note that discharges from all three dams include flows overtopping the dam crest. The depth of overtopping during the 100-year return interval storm is approximately 2.2 feet, 2.1 feet and 1.3 feet for Upper, Middle and Lower South Lake dams, respectively.

3.0 ALTERNATIVES

B&L has prepared hydrologic and hydraulic computations for two dam breach alternatives focused on reducing the maintenance and inspection requirements for the Upper and Middle South Lake Dams. The conceptual design characteristics of each breach are based on the computed SDF for the baseline condition and assume that the design head for each lake will not exceed existing conditions. As a result, the required breach width may be computed directly using the weir flow equation for a rectangular, broad-crested weir (C=2.60). The resulting breach widths to safely convey the SDF for the Upper and Middle South Lake dams have been calculated as 90 feet and 100 feet, respectively. This approach is conservative given that it ignores potential flow in side-slope areas if the breach shape is trapezoidal.

B&L used the computed breach dimensions to develop a hydrologic model for Alternative 1, which assumes the following design requirements:

Upper South Lake

- Design normal pool elevation of 787.7 feet (1-foot higher than Middle South Lake)
- Design head of 2.3 feet with restored dam crest elevation of 790.0 feet (minimum)
- Construction of new earthen broad-crested weir
    - Weir length of approximately 90 feet
    - Invert elevation of 787.7 feet
    - SDF design flood peak elevation of 790.0 feet

Middle South Lake

- Maintains present normal pool elevation at 786.7 feet
- Design head of 2.1 feet with restored dam crest elevation of 788.8 feet (minimum)
- Construction of new non-erodible spillway weir

- Weir length of approximately 100 feet
- Invert elevation of 786.7 feet
- SDF design flood peak elevation of 788.8 feet

The HEC-HMS model results for Alternative 1 are compared to the baseline condition in **Table 3-1**. As shown, the breach of the Upper and Middle dams will result in higher peak discharges in each sub-sequent reservoir, ultimately increasing peak water surface elevations and discharges at Lower South Lake.

Table 3-1: Comparison of Alternative 1 Hydrologic Model Results to Baseline

Reservoir/Dam	100-Year Return Peak Discharge (cfs)	Δ 100-Year Return Peak Discharge (cfs)	100-Year Return Peak Elevation (ft.)	Δ 100-Year Return Peak Elevation (ft.)
Upper South Lake	665	132	789.7	-2.0
Middle South Lake	684	164	788.6	-0.2
Lower South Lake	691	278	784.7	0.3

The risk of higher peak flood elevations and peak discharges at Lower South Lake may be mitigated through the addition of storage above the normal pool elevation on Middle South Lake. B&L developed an additional HEC-HMS model scenario (Alternative 2) that considers added storage to offset potential impacts from the breach of both the Upper and Middle dams. The breach characteristics from Alternative 1 are maintained for the second model scenario, which was executed iteratively to reflect added storage for the first few feet above normal pool until resulting peak water surface elevations on Lower South Lake did not exceed baseline conditions. Approximately 30 acre-feet of additional storage is required between elevations 786.7 feet (normal pool) and 788.0 feet on Middle South Lake to offset increased inflows. HEC-HMS model results for Alternative 2 are compared the baseline condition in **Table 3-2**.

Table 3-2: Comparison of Alternative 2 Hydrologic Model Results to Baseline

Reservoir/Dam	100-Year Return Peak Discharge (cfs)	Δ 100-Year Return Peak Discharge (cfs)	100-Year Return Peak Elevation (ft.)	Δ 100-Year Return Peak Elevation (ft.)
Upper South Lake	665	132	789.7	-2.0
Middle South Lake	477	-43	788.2	-0.6
Lower South Lake	430	10	784.4	0.0

4.0 CONCLUSIONS AND RECOMMENDATIONS

Our initial breach assessment finds that it is conceptually feasible to breach the Upper South Lake dam to the extent that DEC would accept an updated assessment of Hazard Class 'D', eliminating dam safety requirements for the structure. The County's initial requirement to maintain the existing pool elevation of Middle South Lake rules out a change to Hazard Class 'D' for the middle dam since the normal stage of the lake is approximately 4 feet higher in elevation than Lower South Lake. Based on previous

discussions with DEC Dam Safety, impoundment of 1 foot or less above a lower reservoir has generally been accepted in similar situations. However, a Hazard Class 'A' designation may still be achieved for the Middle South Lake dam provided the future spillway configuration for Lower South Lake dam is capable of handling higher peak discharges than the present outlet can safely convey. Additionally, adding storage above the normal pool elevation on Middle and/or Lower South Lake will mitigate flood conditions and reduce the design requirements for the outlet under Lake Louise Drive.

B&L recommends further evaluation of the potential flood impacts that would result from the proposed breach of each dam on properties and infrastructure on Lower South Lake and further downstream. This additional analysis could include:

- Mapping the change in flood inundation limits adjacent to Lower South Lake to see if increased inflows result in new or amplified flood damages.
- Evaluation of stream erosion impacts that could potentially result from increasing peak flows in downstream tributaries.

APPENDIX A
HEC-HMS MODEL REPORTS

Project: Upper___Middle_South_Lake_D
Simulation Run: EA Dup w/ Lower Lake - 100yr
Simulation Start: 29 September 1990, 24:00
Simulation End: 1 October 1990, 12:00

HMS Version: 4.10
Executed: 28 June 2023, 17:20

Global Parameter Summary - Subbasin

Area (MI2)

Element Name	Area (MI2)
Upper Lake DA	0.44
Middle Lake DA	0.17
Lower Lake DA	0.11

Downstream

Element Name	Downstream
Upper Lake DA	Upper South Lake
Middle Lake DA	Middle South Lake
Lower Lake DA	Lower South Lake

Loss Rate: Scs

Element Name	Percent Impervious Area	Curve Number
Upper Lake DA	0	65.97
Middle Lake DA	0	66.06
Lower Lake DA	0	65

Transform: Scs

Element Name	Lag	Unitgraph Type
Upper Lake DA	26.28	Standard
Middle Lake DA	9.78	Standard
Lower Lake DA	33	Standard

Global Results Summary

Hydrologic Element	Drainage Area (MI2)	Peak Discharge (CFS)	Time of Peak	Volume (IN)

Upper Lake DA	0.44	721.06	30Sep1990, 12:30	4.63
Upper South Lake	0.44	532.56	30Sep1990, 12:48	4.54
Middle Lake DA	0.17	400.73	30Sep1990, 12:12	4.65
Middle South Lake	0.61	519.5	30Sep1990, 13:06	4.38
Lower Lake DA	0.11	157.67	30Sep1990, 12:36	4.52
Lower South Lake	0.72	412.94	30Sep1990, 13:42	4
Stream Outlet	0.72	412.94	30Sep1990, 13:42	4

Subbasin: Upper Lake DA

Area (MI2) : 0.44
Downstream : Upper South Lake

Loss Rate: Scs

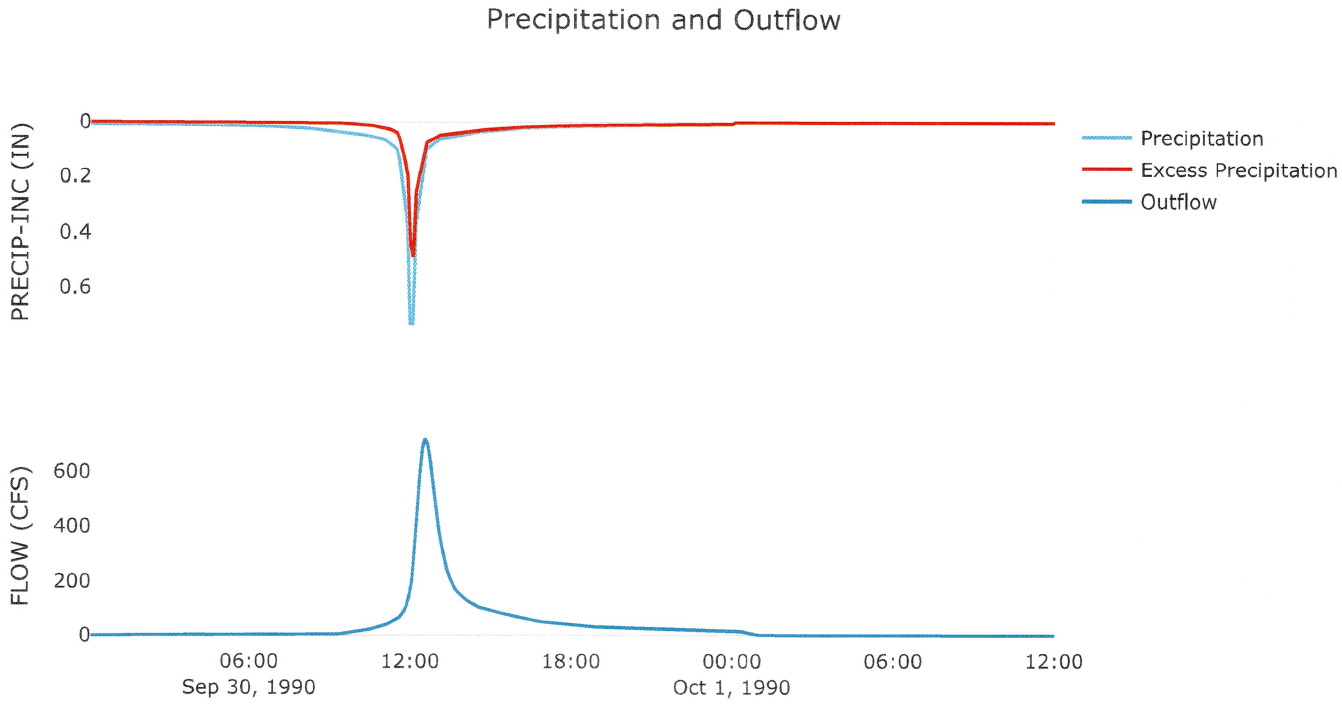
Percent Impervious Area	0
Curve Number	65.97

Transform: Scs

Lag	26.28
Unitgraph Type	Standard

Results: Upper Lake DA

Peak Discharge (CFS)	721.06
Time of Peak Discharge	30Sep1990, 12:30
Volume (IN)	4.63
Precipitation Volume (AC - FT)	206.78
Loss Volume (AC - FT)	97.38
Excess Volume (AC - FT)	109.41
Direct Runoff Volume (AC - FT)	109.41
Baseflow Volume (AC - FT)	0

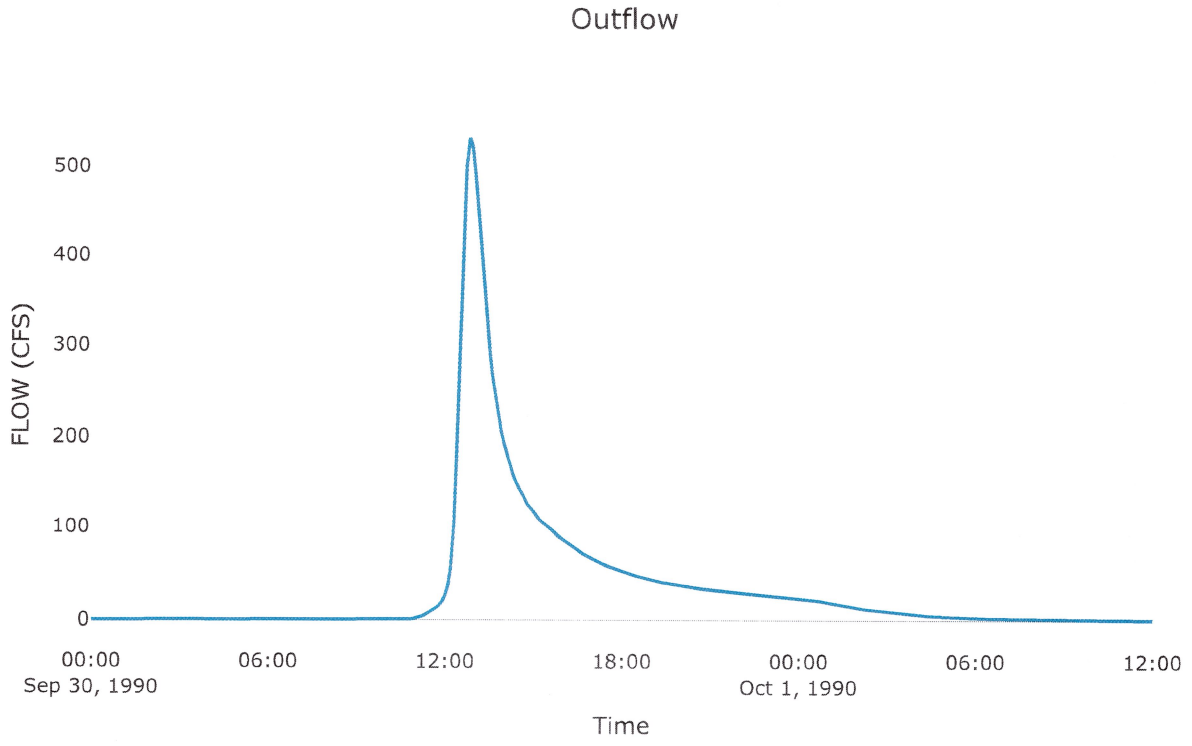


Reservoir: Upper South Lake

Downstream : Middle South Lake

Results: Upper South Lake

Peak Discharge (CFS)	532.56
Time of Peak Discharge	30Sep1990, 12:48
Volume (IN)	4.54
Peak Inflow (CFS)	721.06
Time of Peak Inflow	30Sep1990, 12:30
Inflow Volume (AC - FT)	109.41
Maximum Storage (AC - FT)	48.65
Peak Elevation (FT)	791.69
Discharge Volume (AC - FT)	107.2



Subbasin: Middle Lake DA

Area (MI2) : 0.17
Downstream : Middle South Lake

Loss Rate: Scs

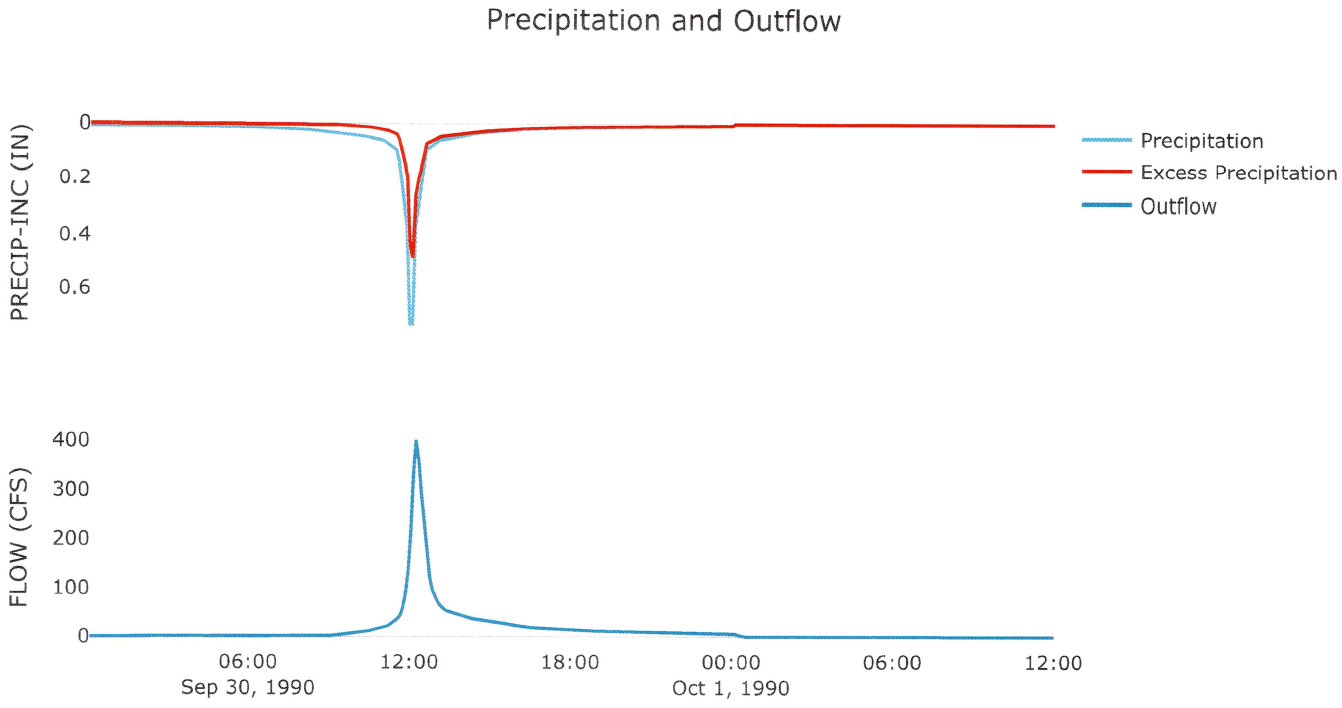
Percent Impervious Area	0
Curve Number	66.06

Transform: Scs

Lag	9.78
Unitgraph Type	Standard

Results: Middle Lake DA

Peak Discharge (CFS)	400.73
Time of Peak Discharge	30Sep1990, 12:12
Volume (IN)	4.65
Precipitation Volume (AC - FT)	78.86
Loss Volume (AC - FT)	37.04
Excess Volume (AC - FT)	41.82
Direct Runoff Volume (AC - FT)	41.82
Baseflow Volume (AC - FT)	0

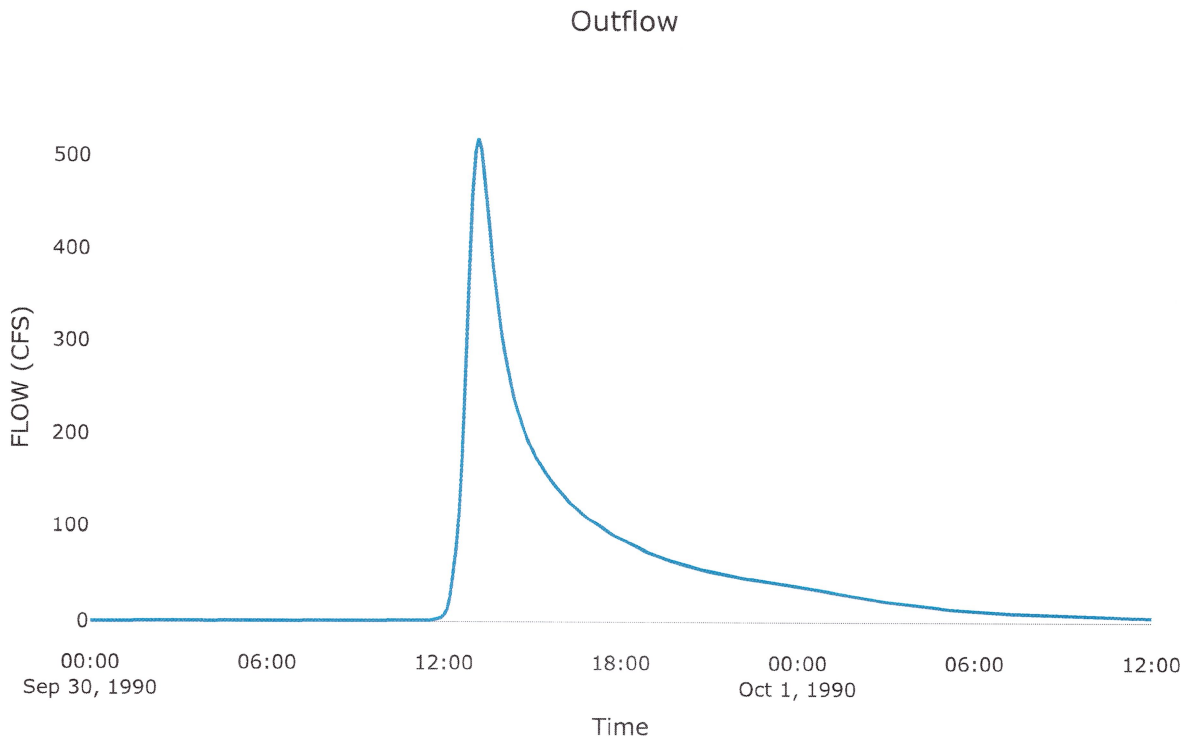


Reservoir: Middle South Lake

Downstream : Lower South Lake

Results: Middle South Lake

Peak Discharge (CFS)	519.5
Time of Peak Discharge	30Sep1990, 13:06
Volume (IN)	4.38
Peak Inflow (CFS)	630.58
Time of Peak Inflow	30Sep1990, 12:48
Inflow Volume (AC - FT)	149.03
Maximum Storage (AC - FT)	110.03
Peak Elevation (FT)	788.83
Discharge Volume (AC - FT)	142.95



Subbasin: Lower Lake DA

Area (MI2) : 0.11
Downstream : Lower South Lake

Loss Rate: Scs

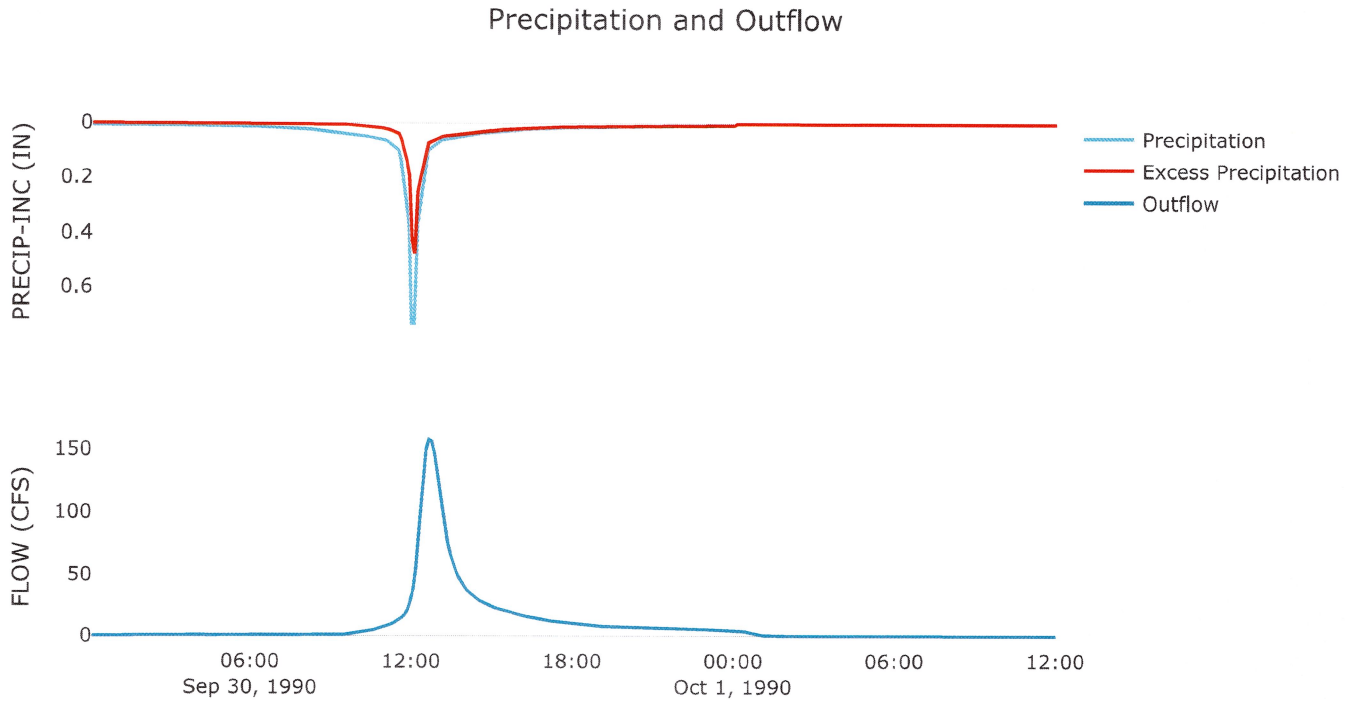
Percent Impervious Area	0
Curve Number	65

Transform: Scs

Lag	33
Unitgraph Type	Standard

Results: Lower Lake DA

Peak Discharge (CFS)	157.67
Time of Peak Discharge	30Sep1990, 12:36
Volume (IN)	4.52
Precipitation Volume (AC - FT)	52.14
Loss Volume (AC - FT)	25.25
Excess Volume (AC - FT)	26.89
Direct Runoff Volume (AC - FT)	26.89
Baseflow Volume (AC - FT)	0

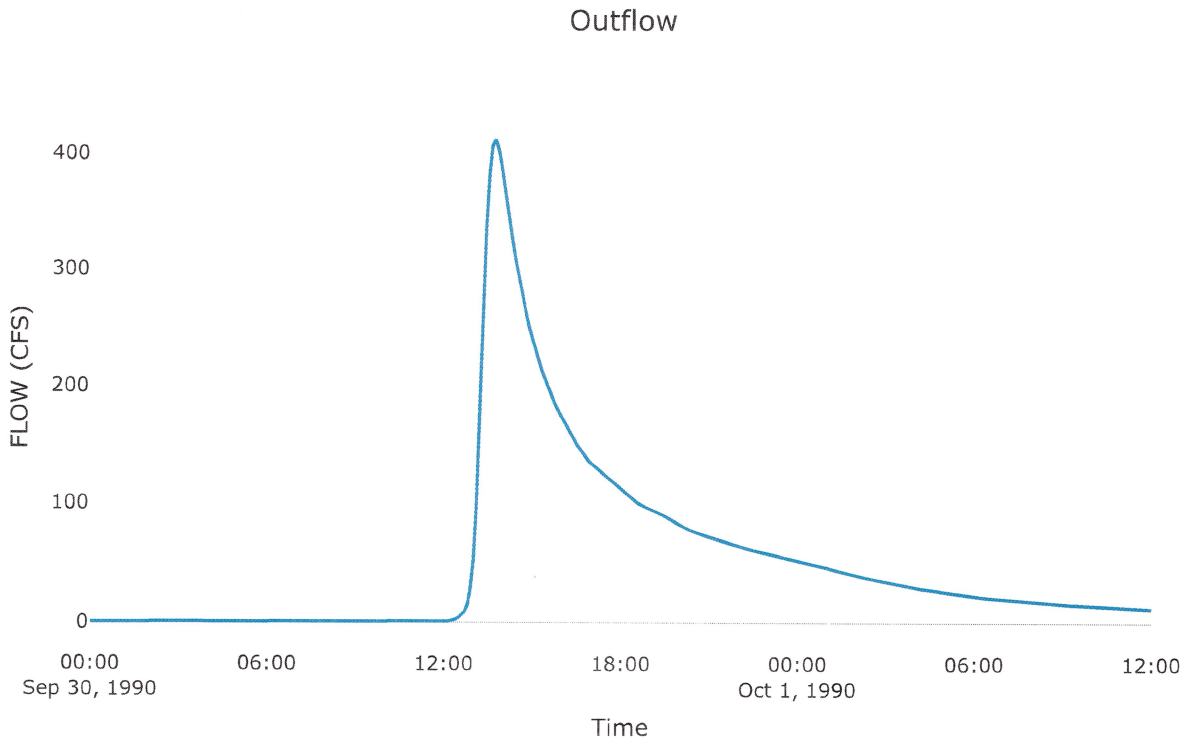


Reservoir: Lower South Lake

Downstream : Stream Outlet

Results: Lower South Lake

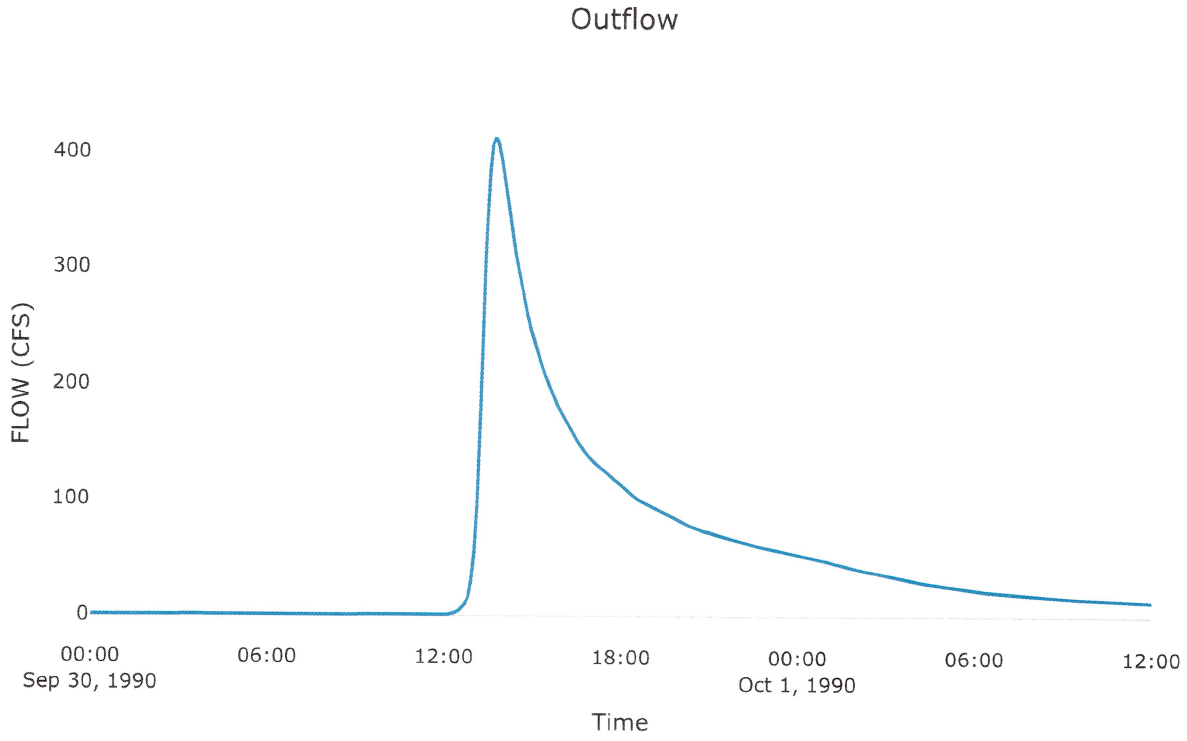
Peak Discharge (CFS)	412.94
Time of Peak Discharge	30Sep1990, 13:42
Volume (IN)	4
Peak Inflow (CFS)	621.59
Time of Peak Inflow	30Sep1990, 13:00
Inflow Volume (AC - FT)	169.83
Maximum Storage (AC - FT)	65.01
Peak Elevation (FT)	784.42
Discharge Volume (AC - FT)	154.34



Sink: Stream Outlet

Results: Stream Outlet

Peak Discharge (CFS)	412.94
Time of Peak Discharge	30Sep1990, 13:42
Volume (IN)	4



Project: Upper___Middle_South_Lake_D
Simulation Run: Breach Upper&MiddleA1- 100yr
Simulation Start: 29 September 1990, 24:00
Simulation End: 1 October 1990, 12:00

HMS Version: 4.10
Executed: 28 June 2023, 17:24

Global Parameter Summary - Subbasin

Area (MI2)

Element Name	Area (MI2)
Upper Lake DA	0.44
Middle Lake DA	0.17
Lower Lake DA	0.11

Downstream

Element Name	Downstream
Upper Lake DA	Upper South Lake
Middle Lake DA	Middle South Lake
Lower Lake DA	Lower South Lake

Loss Rate: Scs

Element Name	Percent Impervious Area	Curve Number
Upper Lake DA	0	65.97
Middle Lake DA	0	66.06
Lower Lake DA	0	65

Transform: Scs

Element Name	Lag	Unitgraph Type
Upper Lake DA	26.28	Standard
Middle Lake DA	9.78	Standard
Lower Lake DA	33	Standard

Global Results Summary

Hydrologic Element	Drainage Area (MI2)	Peak Discharge (CFS)	Time of Peak	Volume (IN)

Upper Lake DA	0.44	721.06	30Sep1990, 12:30	4.63
Upper South Lake	0.44	664.56	30Sep1990, 12:42	4.63
Middle Lake DA	0.17	400.73	30Sep1990, 12:12	4.65
Middle South Lake	0.61	684.09	30Sep1990, 12:54	4.63
Lower Lake DA	0.11	157.67	30Sep1990, 12:36	4.52
Lower South Lake	0.72	690.59	30Sep1990, 13:12	4.31
Stream Outlet	0.72	690.59	30Sep1990, 13:12	4.31

Subbasin: Upper Lake DA

Area (MI2) : 0.44
Downstream : Upper South Lake

Loss Rate: Scs

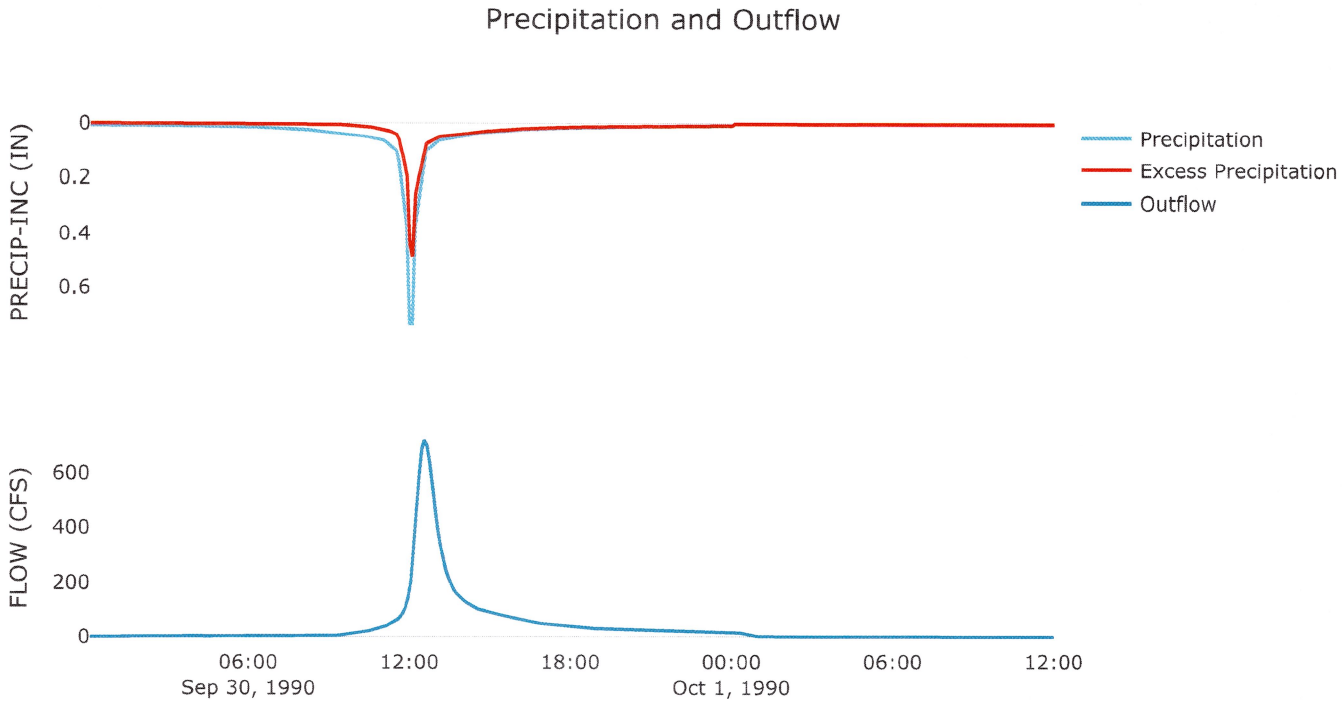
Percent Impervious Area	0
Curve Number	65.97

Transform: Scs

Lag	26.28
Unitgraph Type	Standard

Results: Upper Lake DA

Peak Discharge (CFS)	721.06
Time of Peak Discharge	30Sep1990, 12:30
Volume (IN)	4.63
Precipitation Volume (AC - FT)	206.78
Loss Volume (AC - FT)	97.38
Excess Volume (AC - FT)	109.41
Direct Runoff Volume (AC - FT)	109.41
Baseflow Volume (AC - FT)	0

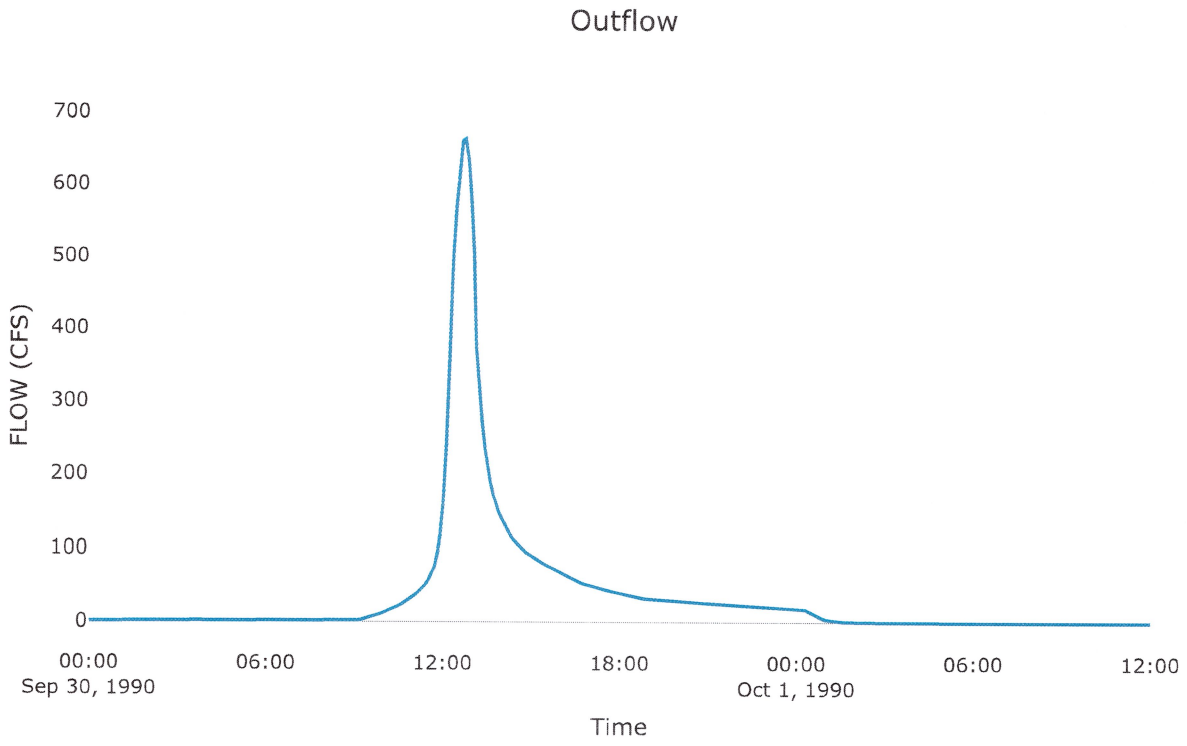


Reservoir: Upper South Lake

Downstream : Middle South Lake

Results: Upper South Lake

Peak Discharge (CFS)	664.56
Time of Peak Discharge	30Sep1990, 12:42
Volume (IN)	4.63
Peak Inflow (CFS)	721.06
Time of Peak Inflow	30Sep1990, 12:30
Inflow Volume (AC - FT)	109.41
Maximum Storage (AC - FT)	21.14
Peak Elevation (FT)	789.68
Discharge Volume (AC - FT)	109.2



Subbasin: Middle Lake DA

Area (MI2) : 0.17
Downstream : Middle South Lake

Loss Rate: Scs

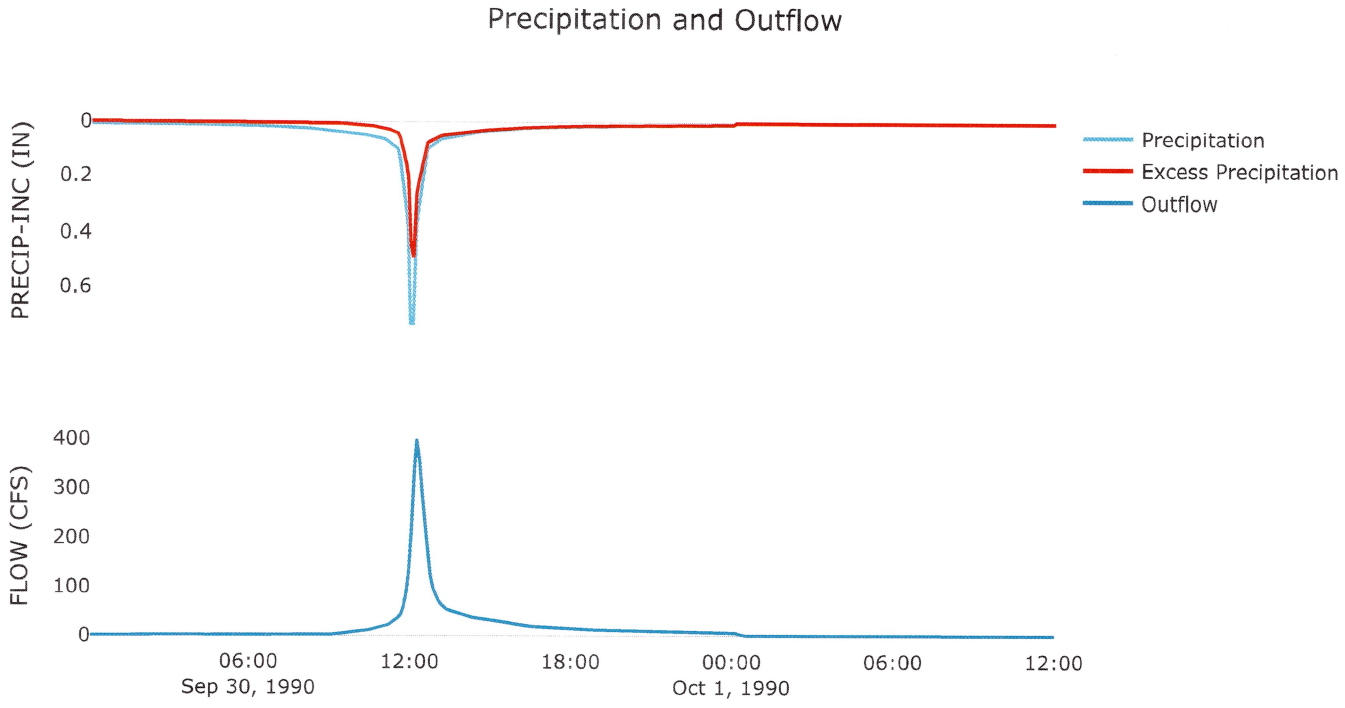
Percent Impervious Area	0
Curve Number	66.06

Transform: Scs

Lag	9.78
Unitgraph Type	Standard

Results: Middle Lake DA

Peak Discharge (CFS)	400.73
Time of Peak Discharge	30Sep1990, 12:12
Volume (IN)	4.65
Precipitation Volume (AC - FT)	78.86
Loss Volume (AC - FT)	37.04
Excess Volume (AC - FT)	41.82
Direct Runoff Volume (AC - FT)	41.82
Baseflow Volume (AC - FT)	0

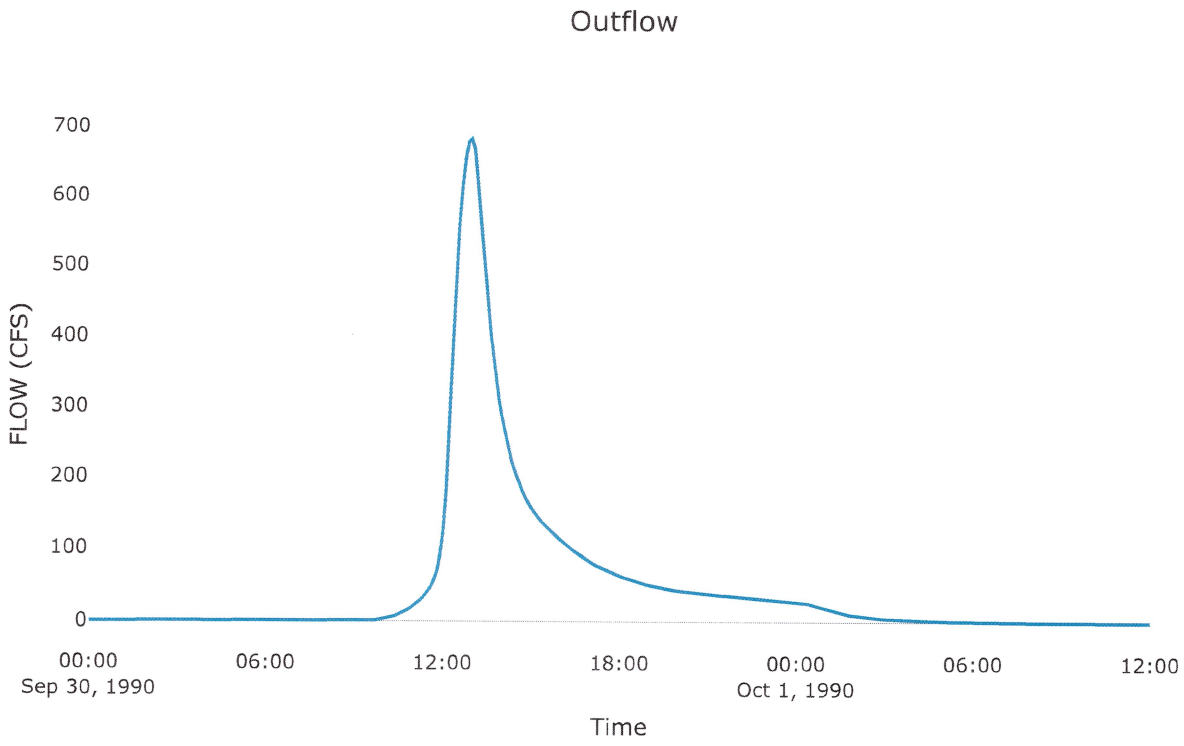


Reservoir: Middle South Lake

Downstream : Lower South Lake

Results: Middle South Lake

Peak Discharge (CFS)	684.09
Time of Peak Discharge	30Sep1990, 12:54
Volume (IN)	4.63
Peak Inflow (CFS)	860.7
Time of Peak Inflow	30Sep1990, 12:18
Inflow Volume (AC - FT)	151.03
Maximum Storage (AC - FT)	105.36
Peak Elevation (FT)	788.57
Discharge Volume (AC - FT)	150.83



Subbasin: Lower Lake DA

Area (MI2) : 0.11
Downstream : Lower South Lake

Loss Rate: Scs

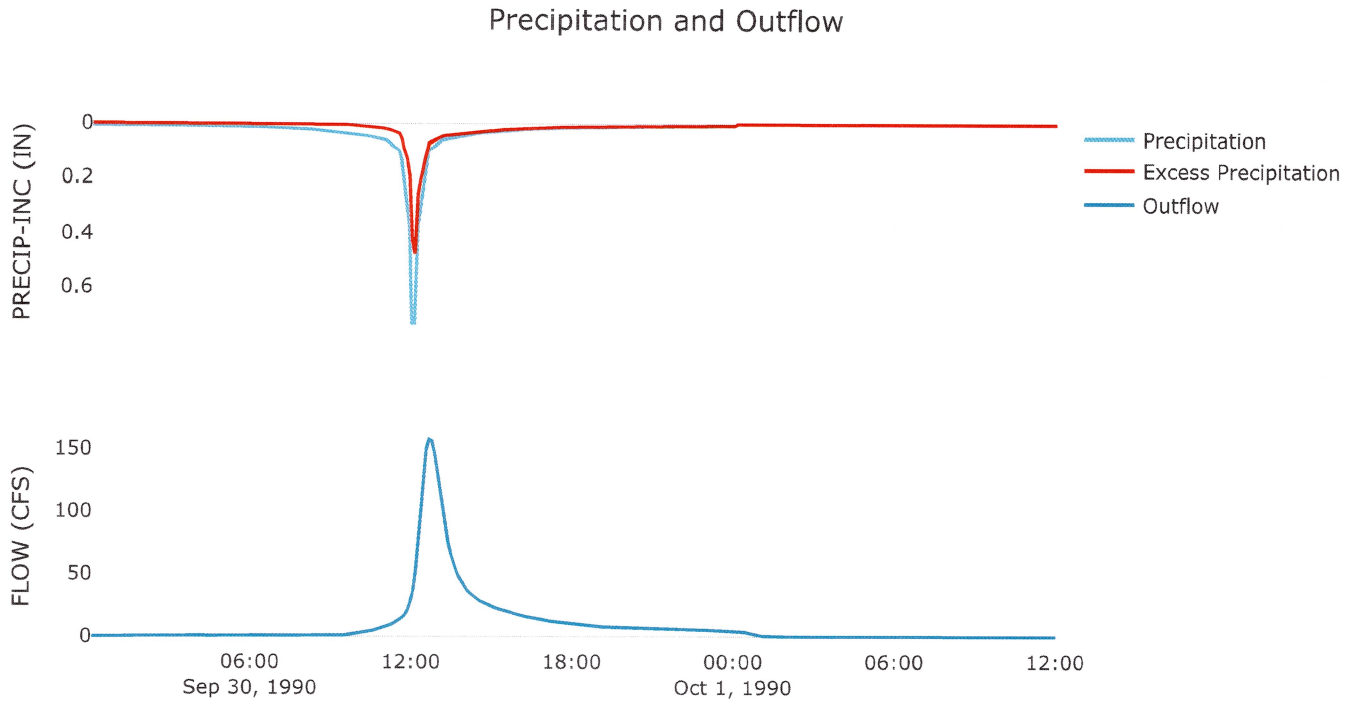
Percent Impervious Area	0
Curve Number	65

Transform: Scs

Lag	33
Unitgraph Type	Standard

Results: Lower Lake DA

Peak Discharge (CFS)	157.67
Time of Peak Discharge	30Sep1990, 12:36
Volume (IN)	4.52
Precipitation Volume (AC - FT)	52.14
Loss Volume (AC - FT)	25.25
Excess Volume (AC - FT)	26.89
Direct Runoff Volume (AC - FT)	26.89
Baseflow Volume (AC - FT)	0

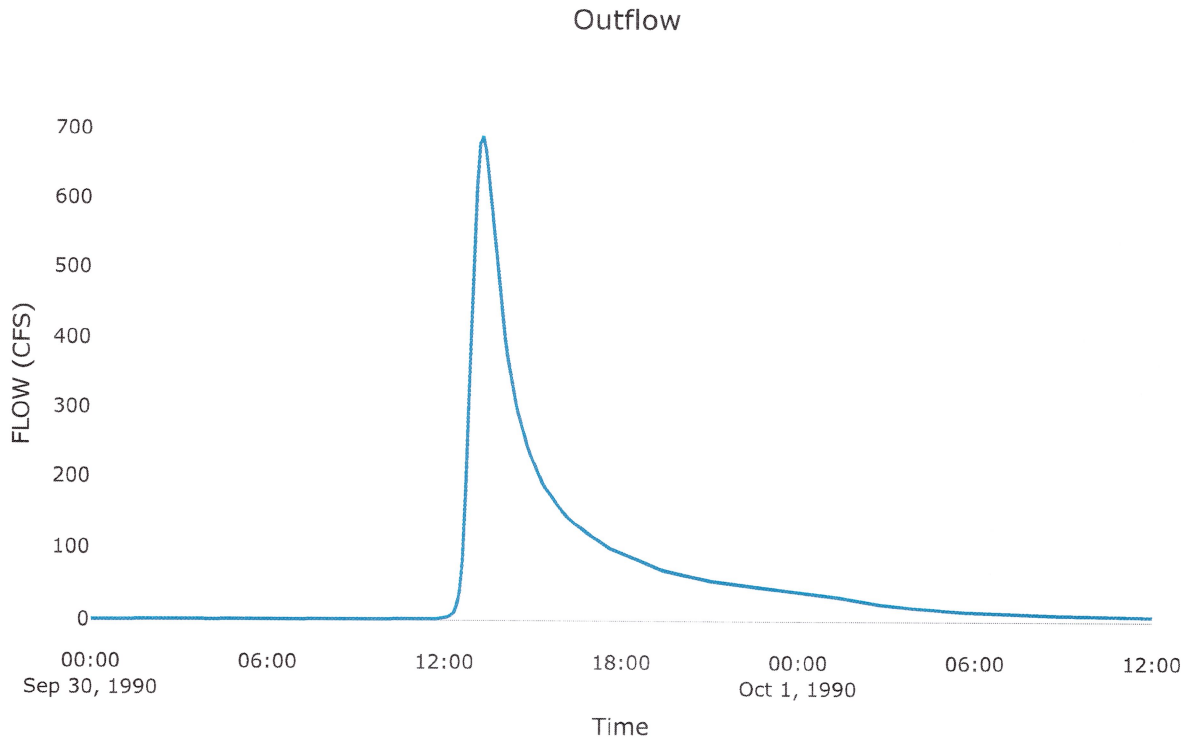


Reservoir: Lower South Lake

Downstream : Stream Outlet

Results: Lower South Lake

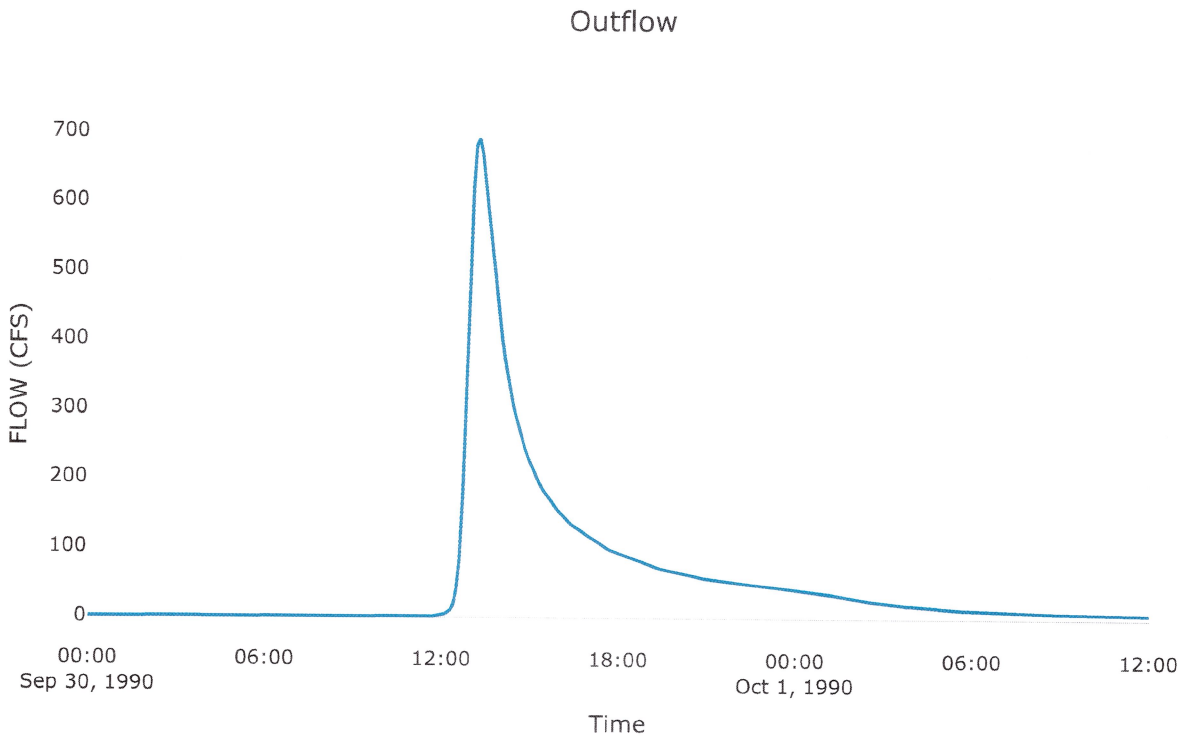
Peak Discharge (CFS)	690.59
Time of Peak Discharge	30Sep1990, 13:12
Volume (IN)	4.31
Peak Inflow (CFS)	827.12
Time of Peak Inflow	30Sep1990, 12:48
Inflow Volume (AC - FT)	177.72
Maximum Storage (AC - FT)	69.75
Peak Elevation (FT)	784.67
Discharge Volume (AC - FT)	166.34



Sink: Stream Outlet

Results: Stream Outlet

Peak Discharge (CFS)	690.59
Time of Peak Discharge	30Sep1990, 13:12
Volume (IN)	4.31



Project: Upper___Middle_South_Lake_D
Simulation Run: Breach Upper&MiddleA2- 100yr
Simulation Start: 29 September 1990, 24:00
Simulation End: 1 October 1990, 12:00

HMS Version: 4.10
Executed: 28 June 2023, 17:28

Global Parameter Summary - Subbasin

Area (MI2)

Element Name	Area (MI2)
Upper Lake DA	0.44
Middle Lake DA	0.17
Lower Lake DA	0.11

Downstream

Element Name	Downstream
Upper Lake DA	Upper South Lake
Middle Lake DA	Middle South Lake
Lower Lake DA	Lower South Lake

Loss Rate: Scs

Element Name	Percent Impervious Area	Curve Number
Upper Lake DA	0	65.97
Middle Lake DA	0	66.06
Lower Lake DA	0	65

Transform: Scs

Element Name	Lag	Unitgraph Type
Upper Lake DA	26.28	Standard
Middle Lake DA	9.78	Standard
Lower Lake DA	33	Standard

Global Results Summary

Hydrologic Element	Drainage Area (MI2)	Peak Discharge (CFS)	Time of Peak	Volume (IN)

Upper Lake DA	0.44	721.06	30Sep1990, 12:30	4.63
Upper South Lake	0.44	664.56	30Sep1990, 12:42	4.63
Middle Lake DA	0.17	400.73	30Sep1990, 12:12	4.65
Middle South Lake	0.61	476.81	30Sep1990, 13:06	4.59
Lower Lake DA	0.11	157.67	30Sep1990, 12:36	4.52
Lower South Lake	0.72	429.78	30Sep1990, 13:36	4.23
Stream Outlet	0.72	429.78	30Sep1990, 13:36	4.23

Subbasin: Upper Lake DA

Area (MI2) : 0.44
Downstream : Upper South Lake

Loss Rate: Scs

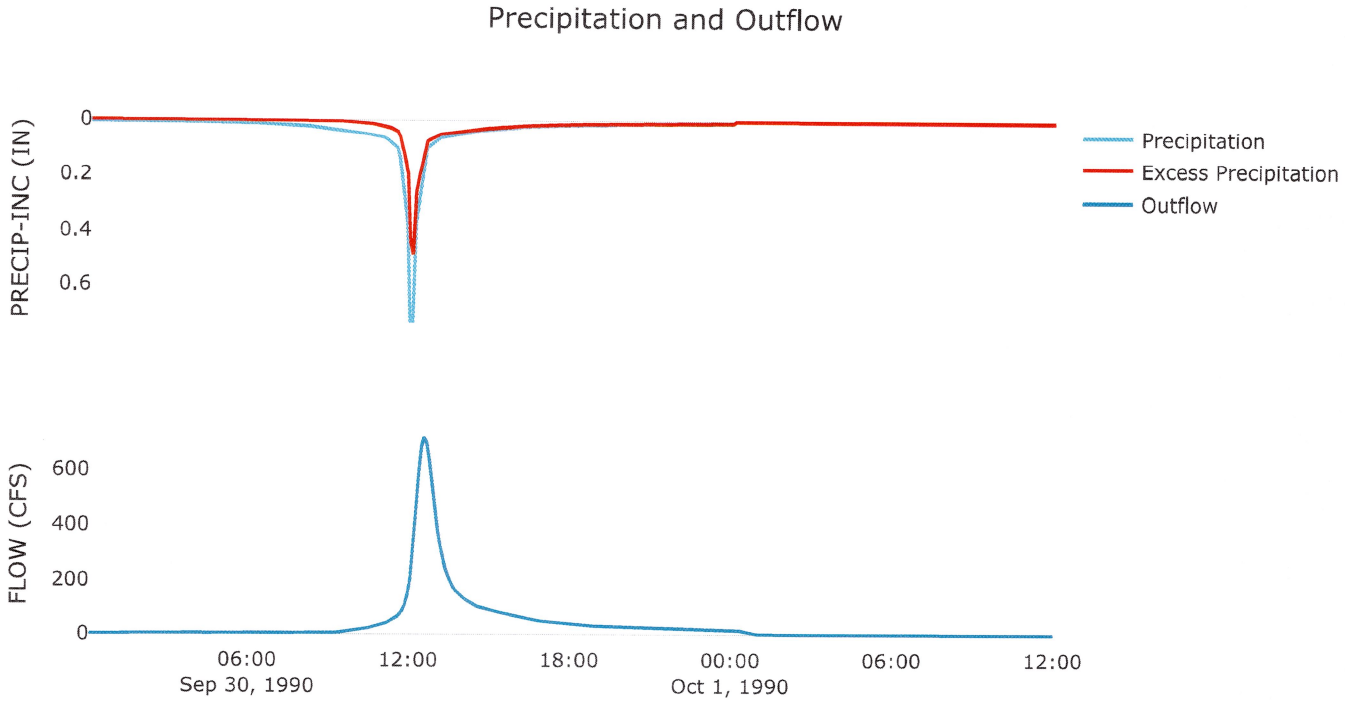
Percent Impervious Area	0
Curve Number	65.97

Transform: Scs

Lag	26.28
Unitgraph Type	Standard

Results: Upper Lake DA

Peak Discharge (CFS)	721.06
Time of Peak Discharge	30Sep1990, 12:30
Volume (IN)	4.63
Precipitation Volume (AC - FT)	206.78
Loss Volume (AC - FT)	97.38
Excess Volume (AC - FT)	109.41
Direct Runoff Volume (AC - FT)	109.41
Baseflow Volume (AC - FT)	0

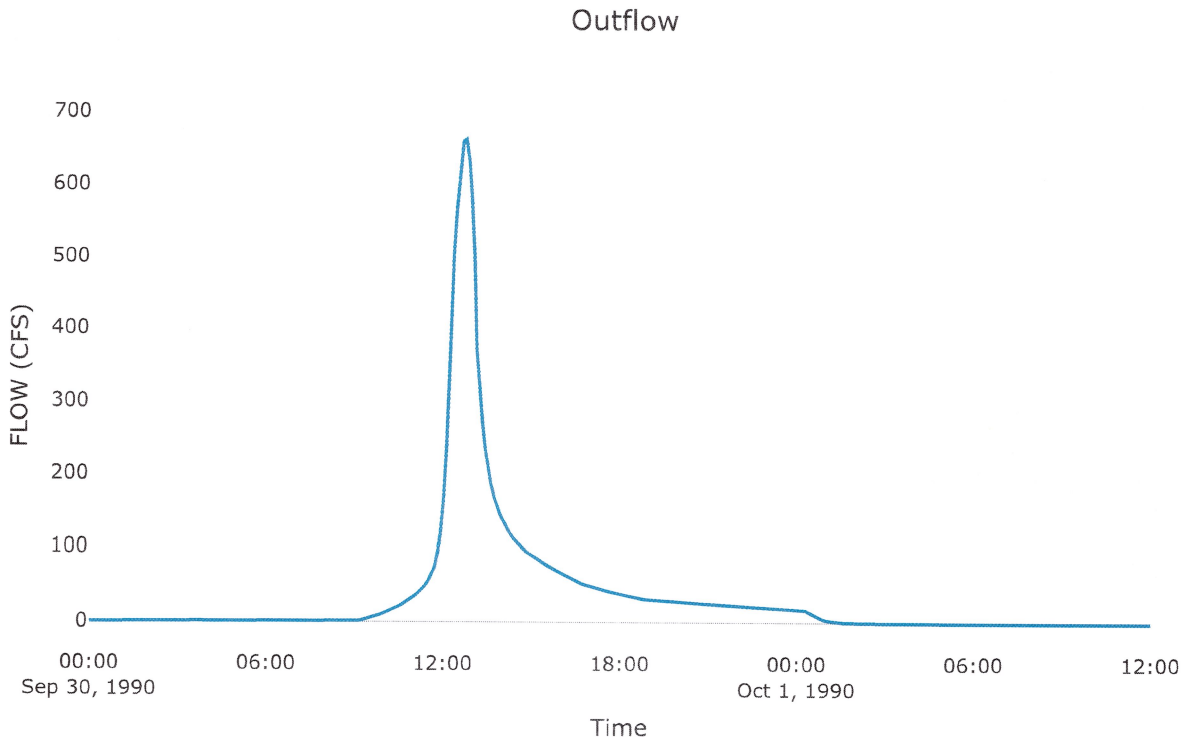


Reservoir: Upper South Lake

Downstream : Middle South Lake

Results: Upper South Lake

Peak Discharge (CFS)	664.56
Time of Peak Discharge	30Sep1990, 12:42
Volume (IN)	4.63
Peak Inflow (CFS)	721.06
Time of Peak Inflow	30Sep1990, 12:30
Inflow Volume (AC - FT)	109.41
Maximum Storage (AC - FT)	21.14
Peak Elevation (FT)	789.68
Discharge Volume (AC - FT)	109.2



Subbasin: Middle Lake DA

Area (MI2) : 0.17
Downstream : Middle South Lake

Loss Rate: Scs

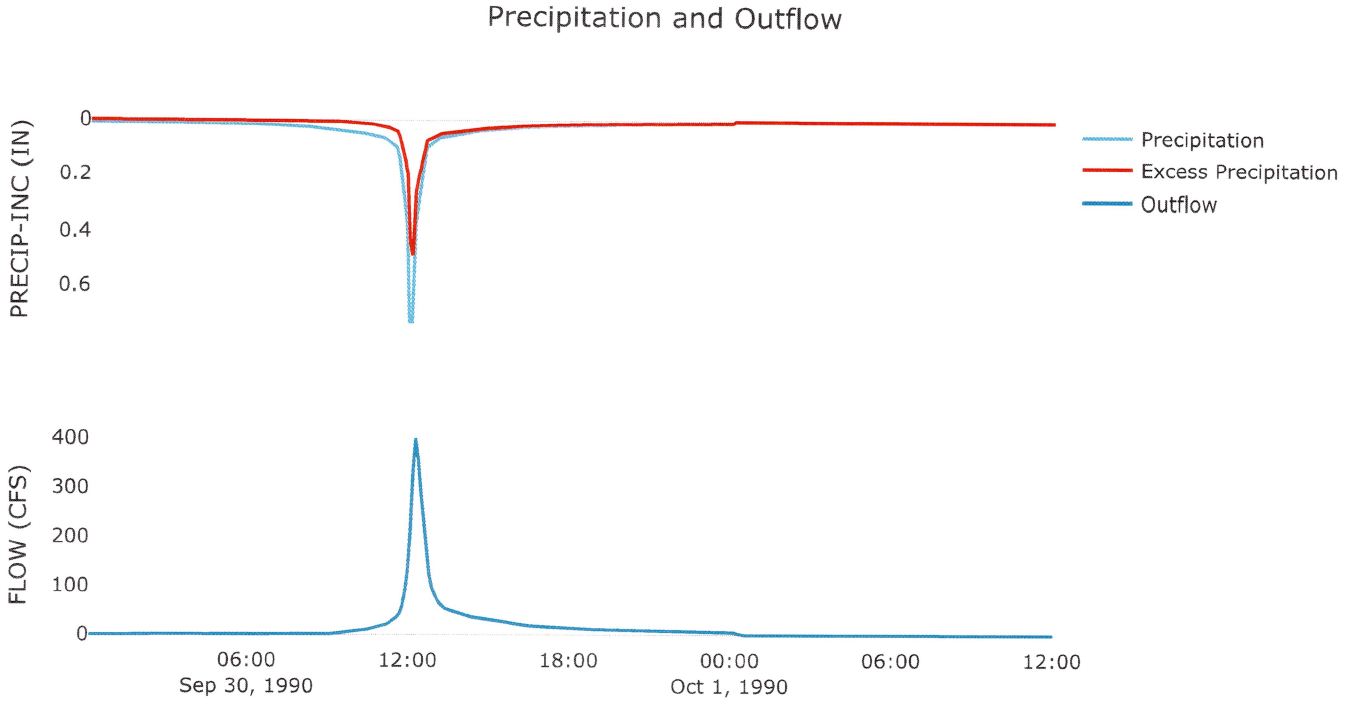
Percent Impervious Area	0
Curve Number	66.06

Transform: Scs

Lag	9.78
Unitgraph Type	Standard

Results: Middle Lake DA

Peak Discharge (CFS)	400.73
Time of Peak Discharge	30Sep1990, 12:12
Volume (IN)	4.65
Precipitation Volume (AC - FT)	78.86
Loss Volume (AC - FT)	37.04
Excess Volume (AC - FT)	41.82
Direct Runoff Volume (AC - FT)	41.82
Baseflow Volume (AC - FT)	0

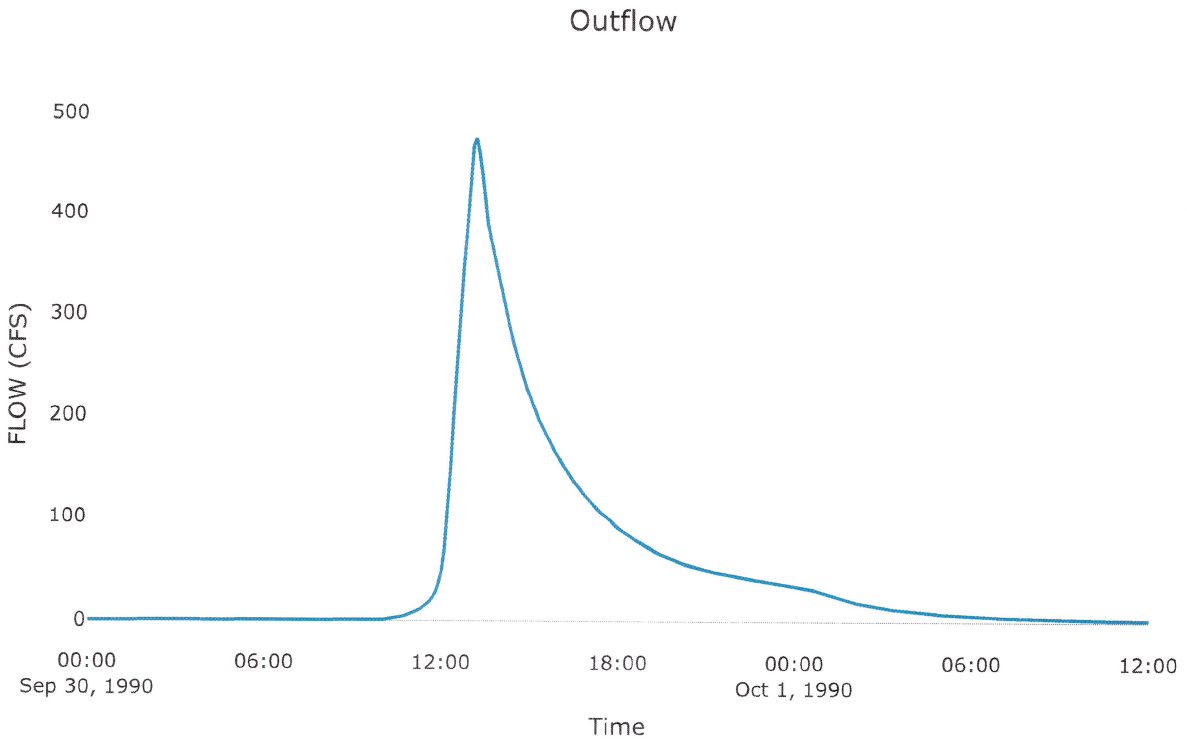


Reservoir: Middle South Lake

Downstream : Lower South Lake

Results: Middle South Lake

Peak Discharge (CFS)	476.81
Time of Peak Discharge	30Sep1990, 13:06
Volume (IN)	4.59
Peak Inflow (CFS)	860.7
Time of Peak Inflow	30Sep1990, 12:18
Inflow Volume (AC - FT)	151.03
Maximum Storage (AC - FT)	128.19
Peak Elevation (FT)	788.17
Discharge Volume (AC - FT)	149.64



Subbasin: Lower Lake DA

Area (MI2) : 0.11
Downstream : Lower South Lake

Loss Rate: Scs

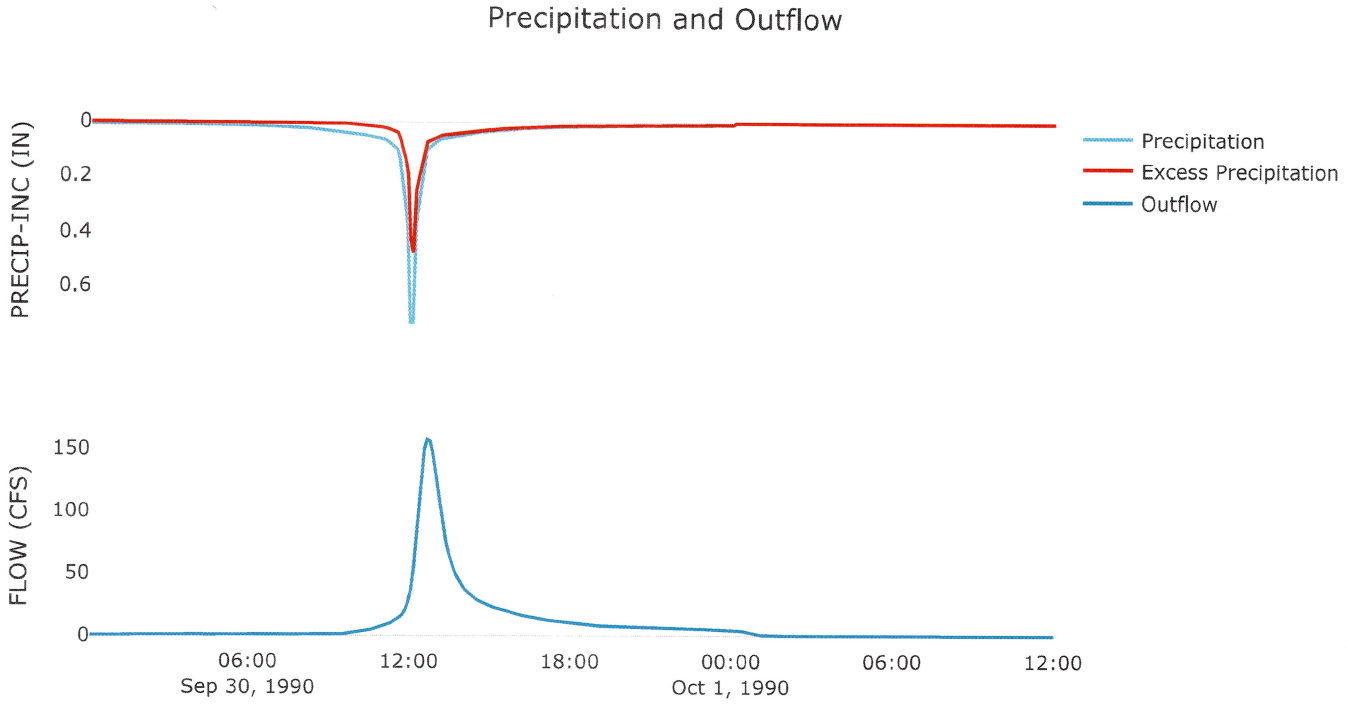
Percent Impervious Area	0
Curve Number	65

Transform: Scs

Lag	33
Unitgraph Type	Standard

Results: Lower Lake DA

Peak Discharge (CFS)	157.67
Time of Peak Discharge	30Sep1990, 12:36
Volume (IN)	4.52
Precipitation Volume (AC - FT)	52.14
Loss Volume (AC - FT)	25.25
Excess Volume (AC - FT)	26.89
Direct Runoff Volume (AC - FT)	26.89
Baseflow Volume (AC - FT)	0

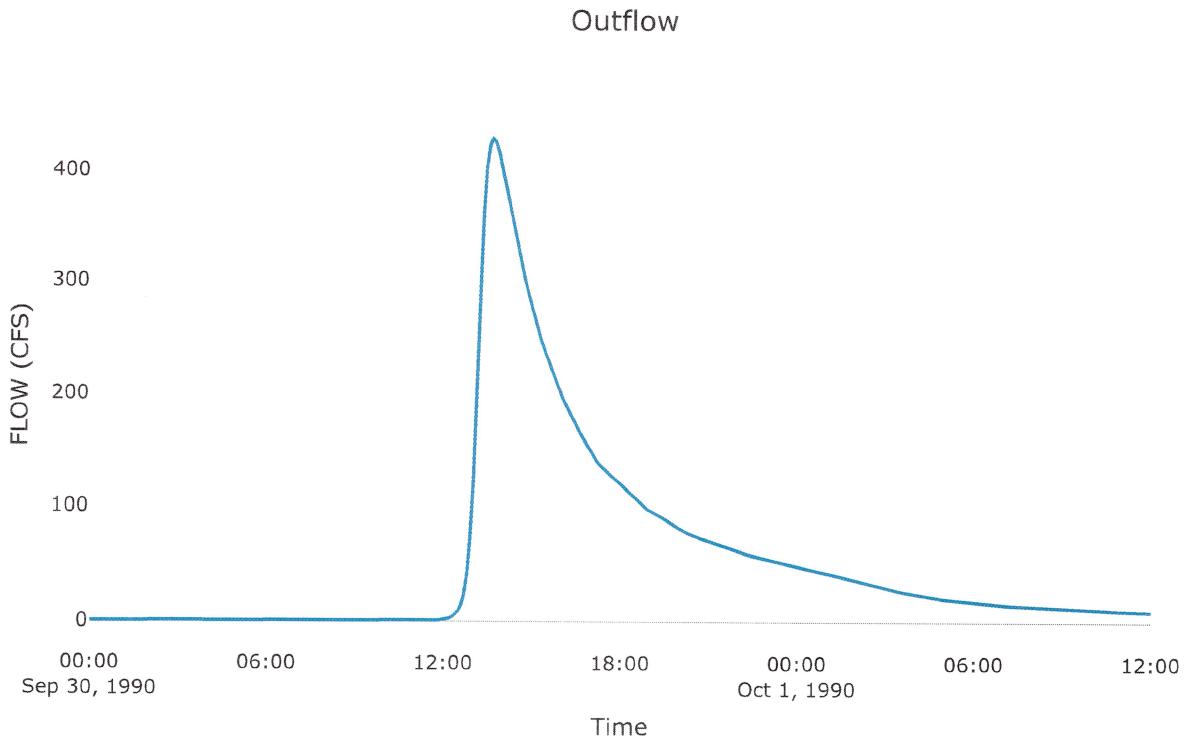


Reservoir: Lower South Lake

Downstream : Stream Outlet

Results: Lower South Lake

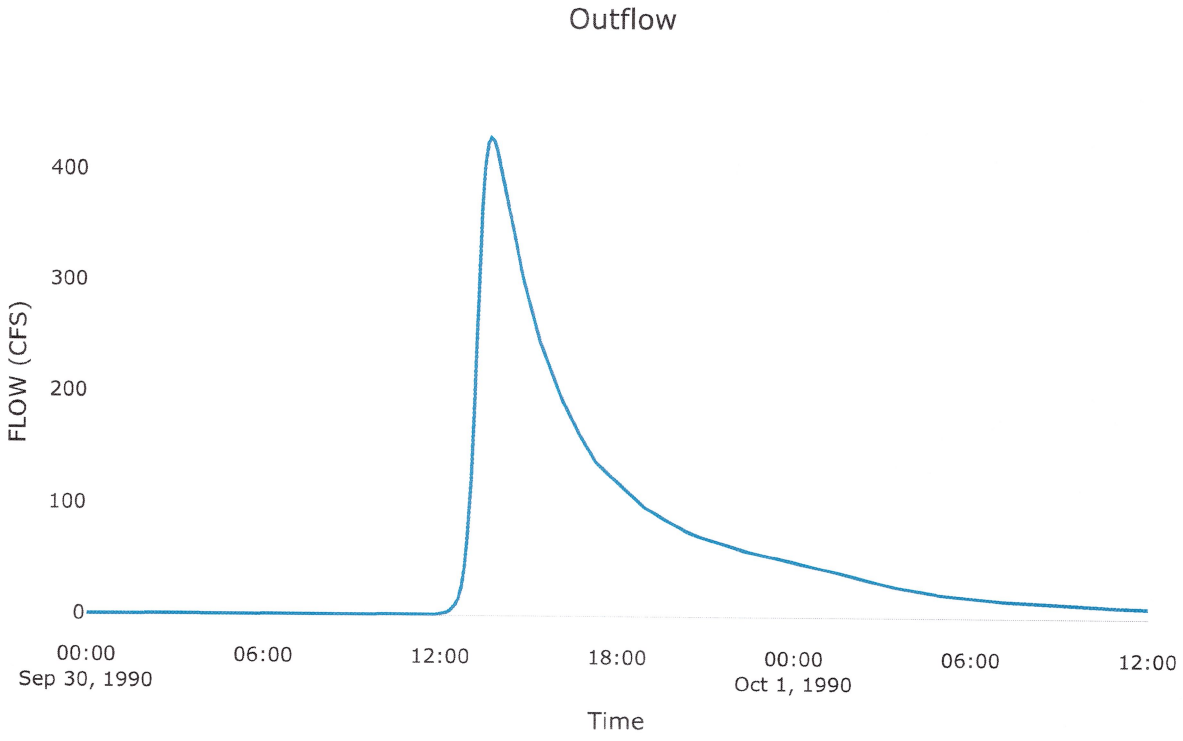
Peak Discharge (CFS)	429.78
Time of Peak Discharge	30Sep1990, 13:36
Volume (IN)	4.23
Peak Inflow (CFS)	585.04
Time of Peak Inflow	30Sep1990, 13:00
Inflow Volume (AC - FT)	176.53
Maximum Storage (AC - FT)	65.36
Peak Elevation (FT)	784.44
Discharge Volume (AC - FT)	163.21



Sink: Stream Outlet

Results: Stream Outlet

Peak Discharge (CFS)	429.78
Time of Peak Discharge	30Sep1990, 13:36
Volume (IN)	4.23



APPENDIX B
CONCEPT PLAN

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mdl
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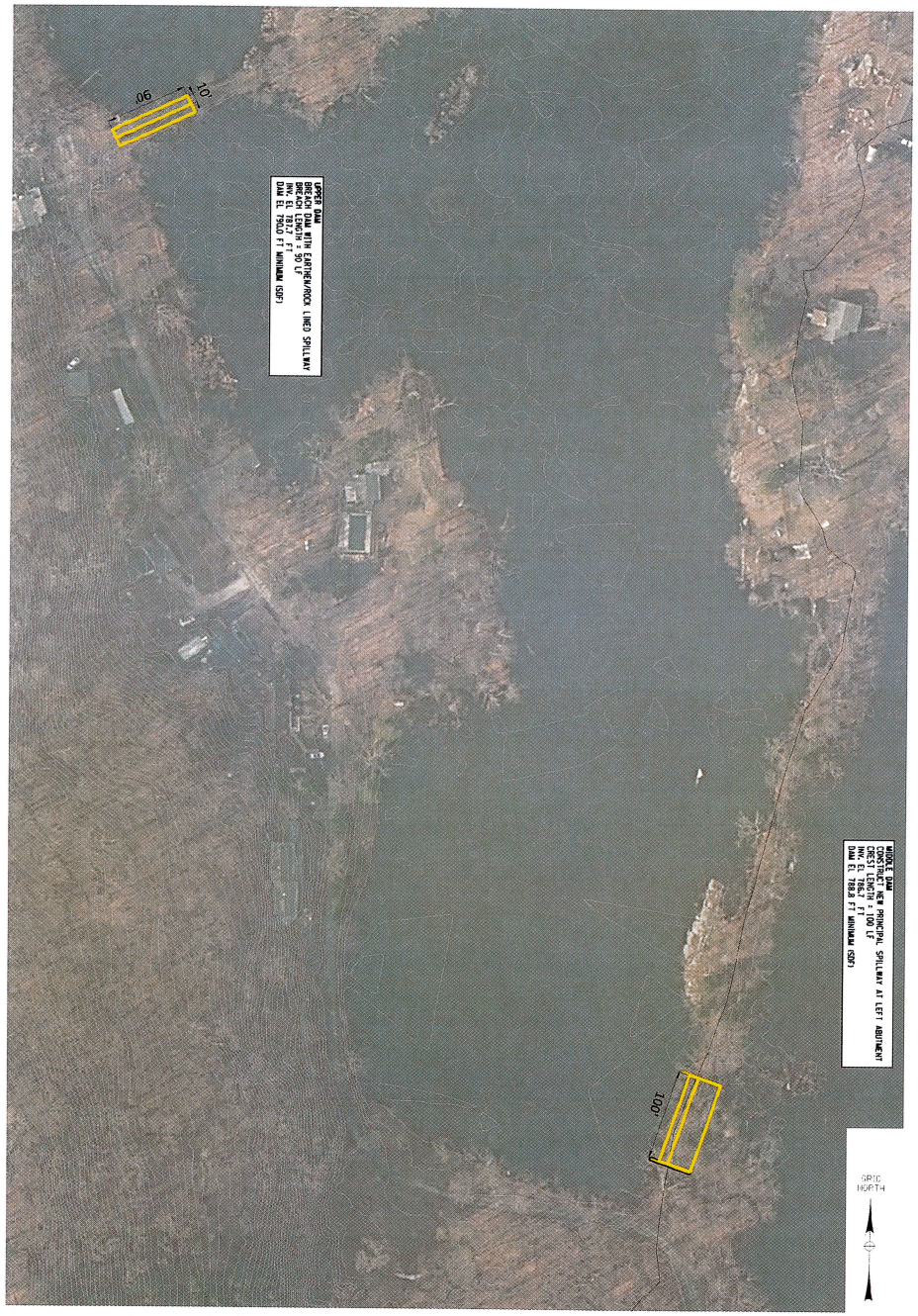
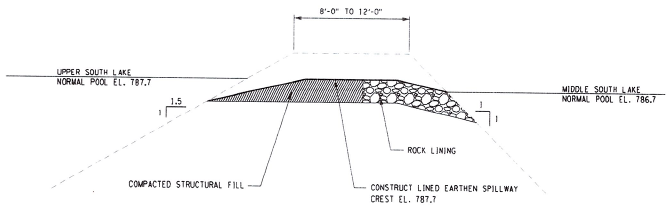
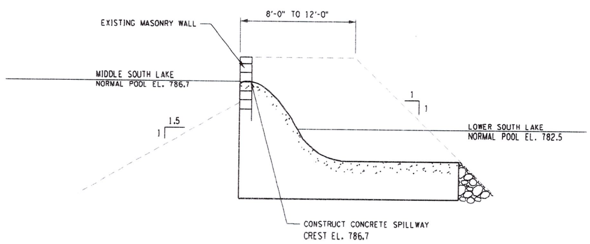
IN CHARGE OF _____ DESIGNED BY _____ CHECKED BY _____ DRAFTED BY _____ CHECKED BY _____



DRAWING: SCHEMATIC PLAN	SCALE: 1"=100' DATE ISSUED: 07/2023	UPPER/MIDDLE SOUTH LAKE DAMS PUTNAM COUNTY	Barton & Loguidice UNAUTHORIZED ALTERATION OR ADDITION TO THIS DRAWING IS A VIOLATION OF THE NEW YORK STATE EDUCATION LAW ARTICLE 145 SECTION 7209	NO. DATE BY REVISION



UPPER SOUTH LAKE DAM
SCALE: 1/8" = 1'-0"



MIDDLE SOUTH LAKE DAM
SCALE: 1/8" = 1'-0"

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IN CHARGE OF ______ DESIGNED BY ______ CHECKED BY ______ DRAFTED BY ______ CHECKED BY ______

NO	DATE	BY	REVISION

Barton & Loguidice

UNAUTHORIZED ALTERATION OR ADDITION TO THIS DRAWING IS A VIOLATION OF THE NEW YORK STATE EDUCATION LAW ARTICLE 145 SECTION 7209

UPPER/MIDDLE SOUTH LAKE DAMS
PUTNAM COUNTY

PROPOSED SECTIONS

SCALE: AS SHOWN
DATE ISSUED: 07 / 2023
DRAWING

Office (845) 306-5595
Fax (845) 225-5130
Email: ceovacant@townofkentny.gov

Sept. 08, 2023

To: Supervisor Jaime McGlasson and Town Board Members of Kent
From: Jack Keher C.E.O. of Vacant Buildings
Re: 11 Hawthorne Rd.

TM.# 33.58-1-34

Enclosed please find the violation issued by the undersigned and bids for correction. The site owner is deceased and the estate is insolvent with no other contacts available.

The following proposals have been submitted;

JB Affordable Lawn Care	$125.00
A.I.M Mowing	$250.00
Lakeside Mowing	Failed to submit a bid

For your consideration and approval.

Respectfully,

Jack Keher
Town of Kent
C.E.O. of Vacant Buildings

Code Enforcement Officer for Vacant Buildings
OF
THE TOWN OF KENT, PUTNAM COUNTY, N.Y. 10512
845-306-5595

ORDER TO REMEDY VIOLATION

Deutsche Bank Nat Trt
1661 Worthington Rd
West Palm Beach,FL 33409

Tax Map #: 33.58-1-34

Date:February 23, 2023

Owner: Deutsche Bank Nat Trt
11 Hawthorne Rd
Kent, NY

Report # C-2023-0031

Complaint:
Property is vacant and has not been registered with PROCHAMPS which is required by the Town of Kent. There are numerous large brannches piled up in rear of the property. Also there is a hole in the roof near the front enterance and a second floor window is not secure and open the the elements. Also the grass and brush is over grown on entire property.

Inspections related to this complaint found the following:

In violation of :

Town of Kent Municipal Code\Chapter 55B - Registrable Property\Chapter 55B-Registrable Property which states

Town of Kent Municipal Code\Chapter 55B - Registrable Property\Chapter 55B-Registrable Property \Section 6.A - Owner of vacant property which states Any owner of vacant property located within the Town shall, within 10 days after the property becomes vacant, register the real property with the Town registry.

Town of Kent Municipal Code\Chapter 55B - Registrable Property\Chapter 55B-Registrable Property \Section 6.B - Registration- which states Initial registration pursuant to this section shall contain, at a minimum the name of the owner, the mailing address of the owner, email address and telephone number of the owner, and if applicable, the name and telephone number of the property manager and said person's address, email address, and telephone number.

Town of Kent Municipal Code\Chapter 55B - Registrable Property\Chapter 55B-Registrable Property \Section 8A - Maintenance which states In addition to the conditions set forth in Chapter 55A of the Town Code regarding property maintenance, properties subject to this article shall be kept free of weeds, overgrown brush, dead vegetation, trash, junk, debris, building materials, any accumulation of newspaper circulars, flyers, notices, except those required by federal, state or local law, discarded personal items including, but not limited to, furniture, clothing, large and small appliances, printed material, or any other items that give the appearance that the property is abandoned.

Town of Kent Municipal Code\Chapter 55B - Registrable Property\Chapter 55B-Registrable Property \Section 9B- Secure Manner- which states A "secure manner" shall include, but not be limited to, the closure and locking of windows, doors, gates and other openings of such size that may allow a child to access the interior of the property or structure. Broken windows, doors, gates, and other openings of such size that may allow a child to access the interior of the property or structure must be repaired. Broken windows shall be secured by reglazing of the window.

Town of Kent Municipal Code\Chapter 55B - Registrable Property\Chapter 55B-Registrable Property \Section6.D - Property sold or Transfer which states If the property is sold or transferred, the new owner is

subject to all the terms of this article. Within 10 days of the transfer, the new owner shall register the vacant property or update the existing registration. The previous owner(s) will not be released from the responsibility of paying all previous unpaid fees, fines, and penalties accrued during that owner's involvement with the vacant property.

You are hereby directed and ordered to remedy the violations by:3/31/2023

Failure to remedy the condition aforesaid and to comply with the applicable provisions of the law may constitute an offense punishable by fine or imprisonment or both.

If you have any further questions, please feel free to contact me at 845-225-3900.

Respectfully,

John Keher
C.E.O. Vacant Buildings
Town of Kent

Town of Kent
POLICE DEPARTMENT

40 SYBIL'S CROSSING, KENT LAKES, NEW YORK 10512

Address All Communications
To: Chief of Police
kentpolice@townofkentny.gov

Emergency: (845) 225-4600
Office: (845) 225-5646
Fax: (845) 306-5288

Sept.1, 2023

Supervisor McGlasson & Kent Town Board
Town of Kent Administrative Offices
25 Sybil's Crossing
Kent lakes, NY 10512

Dear Supervisor McGlasson & Kent Town Board:

The Town of Kent Police Department respectfully requests permission to purchase a "Radio Repeater System" too replace the old system (at least 15 years old and no longer supported by software updates) that we currently lease from NYCOMCO. We are in the process of renegotiating the current lease with NYCOMCO and the reduction in the lease payment will pay for the new Radio Repeater over the course of the repeater's lifetime. Officer Gasparrini worked with Metrocom Radio and got a quote using (New York State Municipal Bid Contract – NYS Contract PT68722).
Attached is a quote outlining all of the equipment that is included in the package.

I would like to take this opportunity to thank you in advance.

Respectfully,

Kevin R. Owens

Chief Kevin R Owens

Kent, Town of

05/08/2023

MOTOROLA SOLUTIONS DRAFT QUOTE-2155971

05/08/2023

Kent, Town of
25 Sybil's Crossing
Carmel, NY 10512

Dear Steve Gasparrini,

Motorola Solutions is pleased to present Kent, Town of with this quote for quality communications equipment and services. The development of this quote provided us the opportunity to evaluate your requirements and propose a solution to best fulfill your communications needs.

This information is provided to assist you in your evaluation process. Our goal is to provide Kent, Town of with the best products and services available in the communications industry. Please direct any questions to Kevin Ronald at kevin@metrocomradio.com.

We thank you for the opportunity to provide you with premier communications and look forward to your review and feedback regarding this quote.

Sincerely,

Kevin Ronald

Motorola Solutions Manufacturer's Representative

Billing Address:
Kent, Town of
25 Sybil's Crossing
Carmel, NY 10512
US

Quote Date:05/08/2023
Expiration Date:07/07/2023
Quote Created By:
Kevin Ronald
kevin@metrocomradio.com

End Customer:
Kent, Town of
Steve Gasparrini
sgasparrini@townofkentny.gov
845-255-4600

NYS Contract PT68722
Includes programming and tuning.
Does not include installation or batteries.
Misc is for a locking cabinet.

Line #	Item Number	Description	Qty	List Price	Sale Price	Ext. Sale Price
	GTR 8000 Base Radio					
1	T7039A	GTR 8000 BASE RADIO	1	$0.00	$0.00	$0.00
1a	X265AM	ADD: BR PRESELECTOR, (150-174 MHZ)	1	$500.00	$325.74	$325.74
1b	CA03863AA	ADD: ASTRO SYSTEM RELEASE 2022.1	1	$0.00	$0.00	$0.00
1c	CA01400AA	ADD: POWER CABLE, DC	1	$0.00	$0.00	$0.00
1d	X182CB	ADD: DUPLEXER, 144-160 MHZ	1	$1,380.00	$899.04	$899.04
1e	CA01949AA	ADD: ANALOG ONLY CONV SW	1	$7,450.00	$4,853.49	$4,853.49
1f	X530BG	ADD: VHF (136-174 MHZ)	1	$6,300.00	$4,104.29	$4,104.29
1g	CA01564AA	INC: CABLE,PRESELECTOR, V/UHF I/O	1	$0.00	$0.00	$0.00
1h	X676BI	ADD: EXT DUAL CIRCULATOR, 144-160	1	$1,500.00	$977.21	$977.21
1i	CA02446AA	ADD: G-SERIES INDOOR CABINET 15RU	1	$1,250.00	$814.34	$814.34

Line #	Item Number	Description	Qty	List Price	Sale Price	Ext. Sale Price
1j	CA00975AA	ADD: BATTERY TEMP SENSOR EXT CABLE	1	$200.00	$130.29	$130.29
	Product Services					
2	LSV00Q00202A	DEVICE PROGRAMMING	1	$857.14	$857.14	$857.14
3	LSV00Q01073A	DEVICE MISCELLANEOUS DEVICE PARTS/EQUIPMENT	1	$1,538.46	$1,538.46	$1,538.46

Grand Total $14,500.00(USD)

Notes:

- Unless otherwise noted, this quote excludes sales tax or other applicable taxes (such as Goods and Services Tax, sales tax, Value Added Tax and other taxes of a similar nature). Any tax the customer is subject to will be added to invoices.